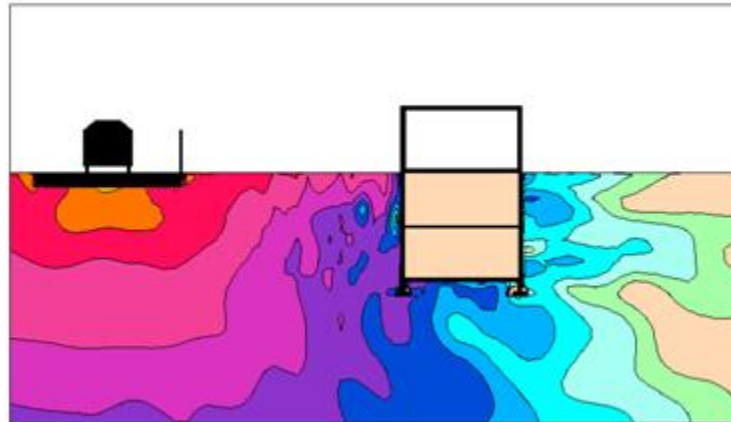


Outils de modélisation de la propagation couplée sol-structure

Philippe JEAN, Michel VILLOT



CSTB
le futur en construction

Introduction

Problème

source : mesure / modèles recalés

Propagation: modélisation des sols

Transfert aux structures: type de contact, 2D, 3D

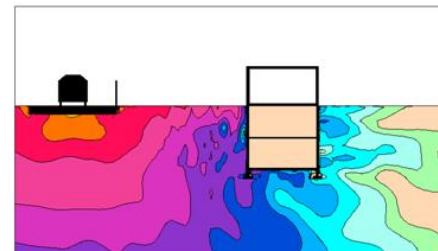
Propagation dans les structures

Rayonnement dans les locaux

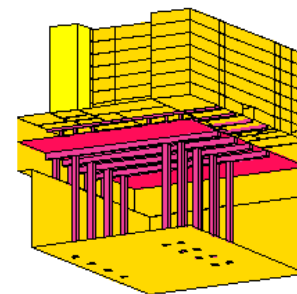
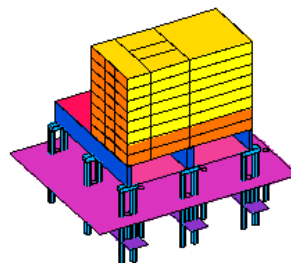
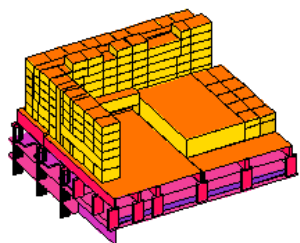
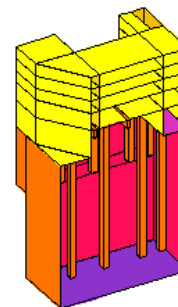
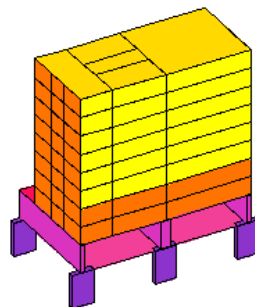
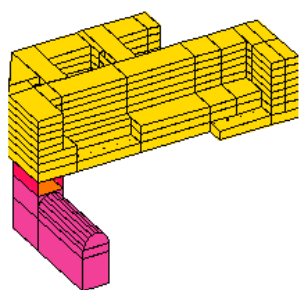
Gêne: tactile, auditive

Indicateurs

Modèles: Energétiques, FEM/BEM, mixtes, mobilités,...



Approche énergétique (SEA) Statistical Energy Analysis



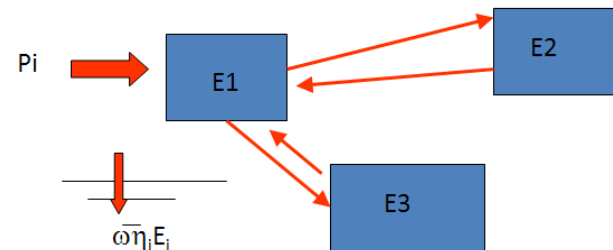
SEA : Principe

Décomposition en systèmes : plaques/ poutres/ poteaux/ volumes

Energies moyennes (F,L,T) par système et par bande de fq (1/3 octave)

Bilan de puissance

$$P_i = \omega \eta_i E_i + \sum \omega \eta_{ij} (E_i / \eta_i - E_j / \eta_j)$$



$$\begin{pmatrix} \eta_{1+} & -\eta_{21} & -\eta_{31} \\ \eta_{12+} & \eta_{2+} & 0 \\ \eta_{13} & \eta_{21} & \eta_{3+} \end{pmatrix} \begin{pmatrix} E1 \\ E2 \\ E3 \end{pmatrix} = \begin{pmatrix} P_i/\omega \\ 0 \\ 0 \end{pmatrix}$$

SEA : limites

Il faut une densité modale suffisante

Problème aux basses fréquences pour les ondes longitudinales
ondes de flexion > 50 Hz

⇒ Modèles mixtes SEA/ modal / ondes

Modèles adaptés aux Basses fréquences: FEM / BEM

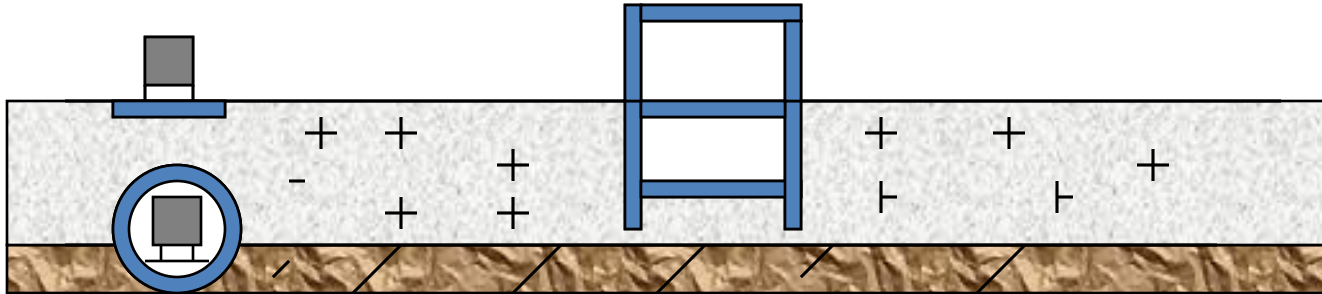
Les méthodes FEM/BEM Logiciel MEFISSTO



FEM : Finite Element Method

BEM : Boundary Element method

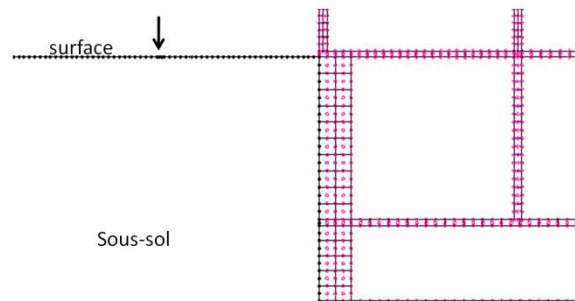
Interaction Sols/Structures (2D et 2.5D)



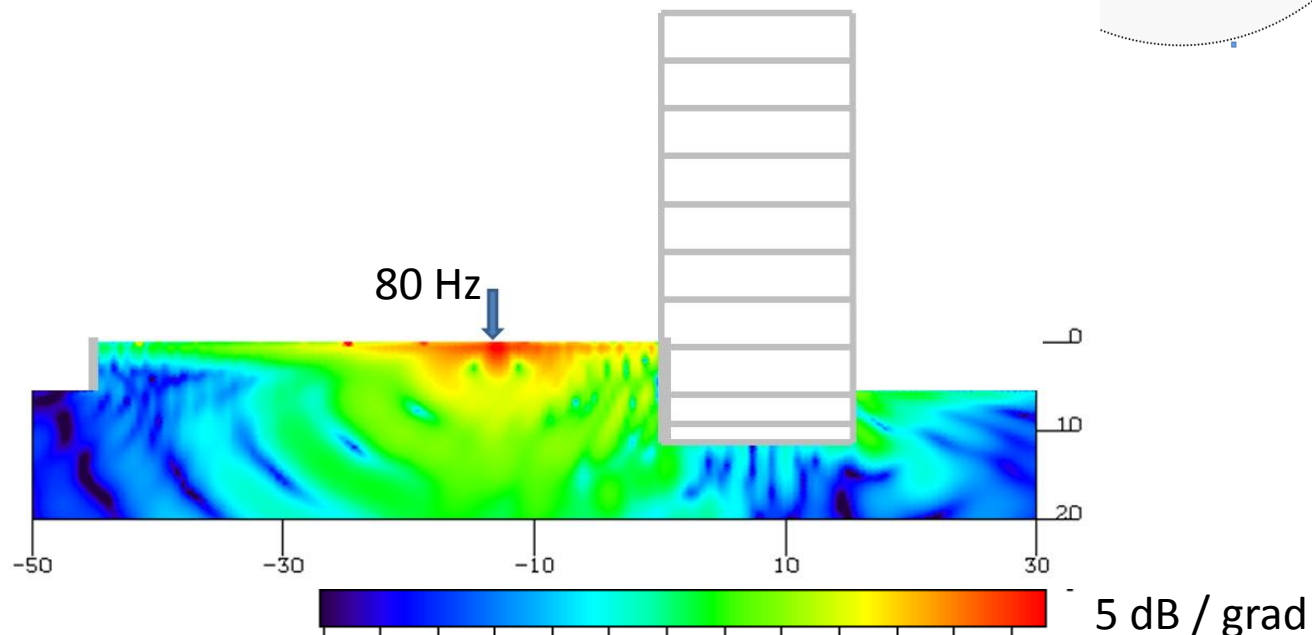
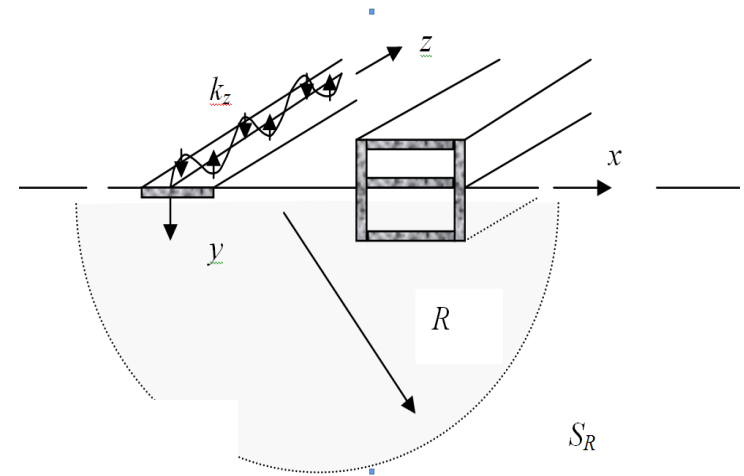
$$\bar{u}(M). \bar{I}(M) = \int_S [\bar{T}(Q, M). \bar{u}(Q) - \bar{G}(Q, M). \bar{t}(Q)] dS + \bar{h}(M)$$

- Séparation en sous-domaines
- Représentation intégrale BEM (collocation) (sols ou structure épaisses)
- ou FEM: condensation aux frontières (structure ou portions de sols)
- Continuité des déplacements et/ou des contraintes aux interfaces

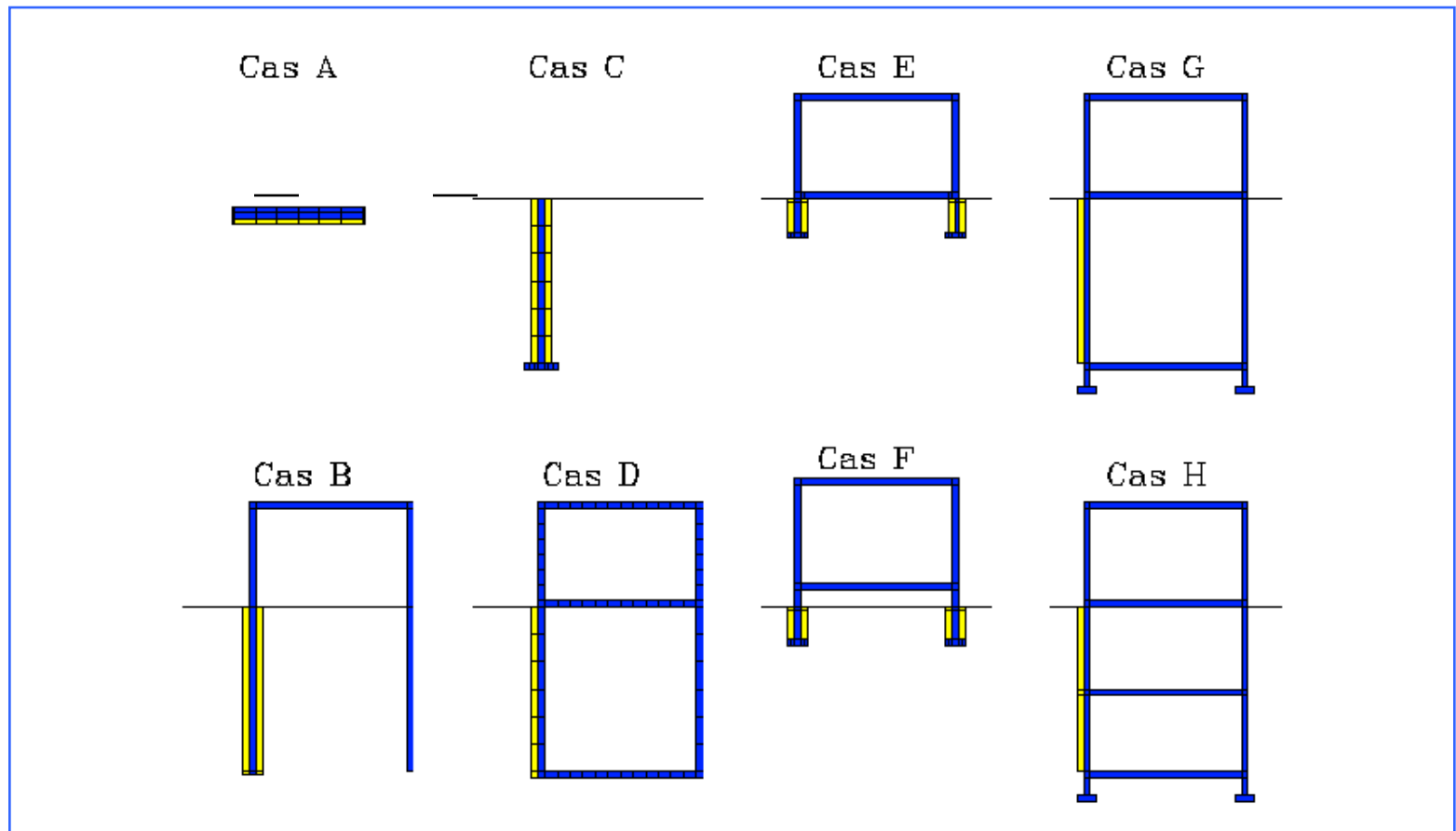
Les méthodes FEM/BEM

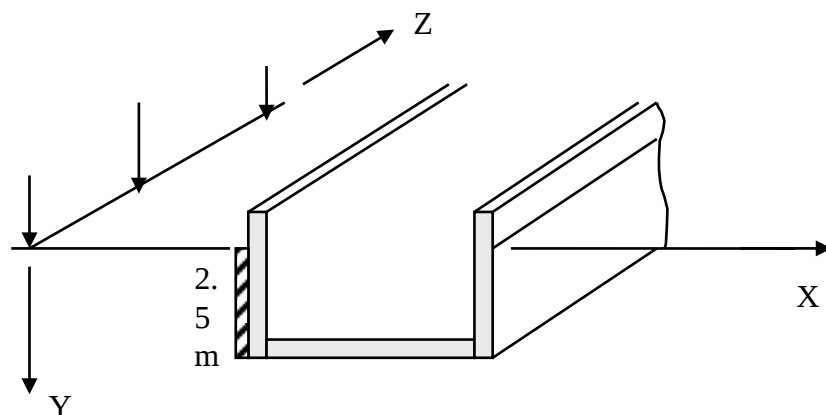


2.5D



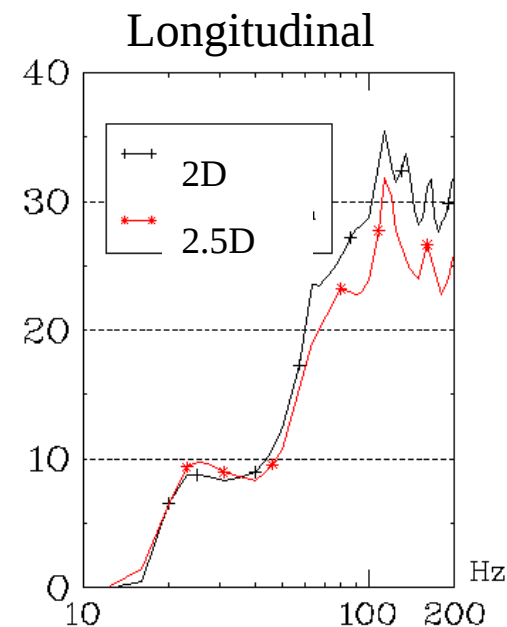
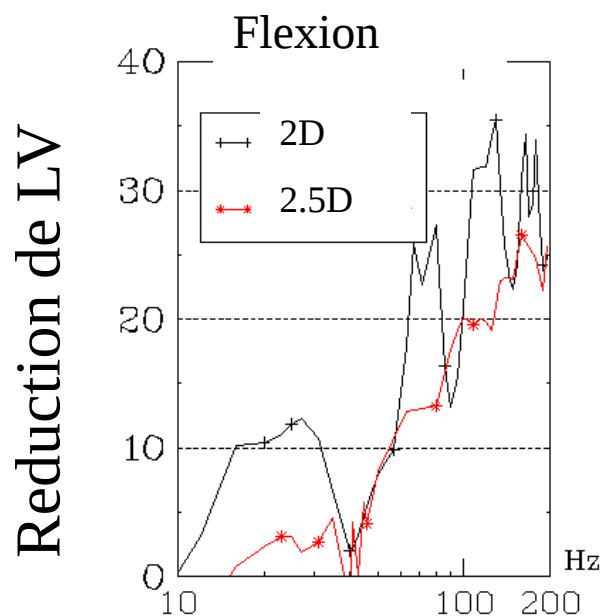
Protection des fondations *(financement ADEME)*





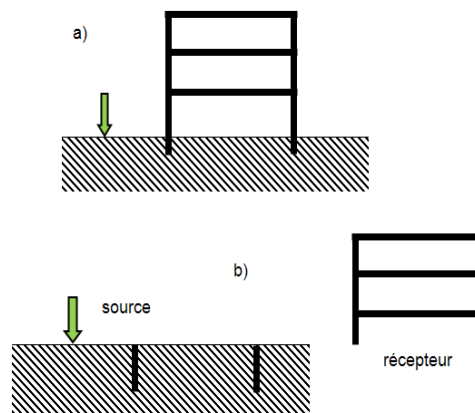
Vérification expérimentale au CSTB

Efficacité
du doublage

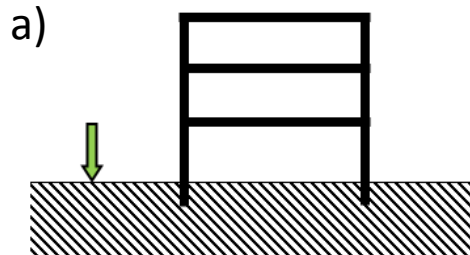


Approche par mobilités

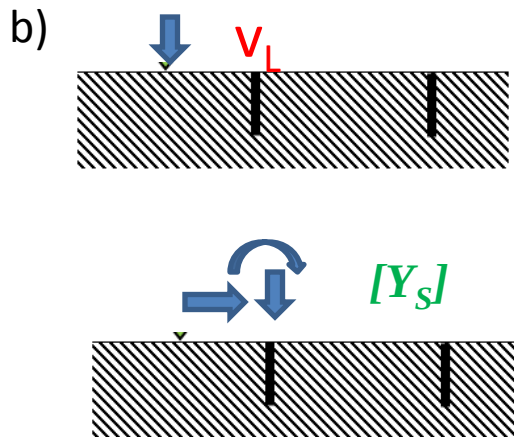
Thèse Pierre ROPARS



PRINCIPE



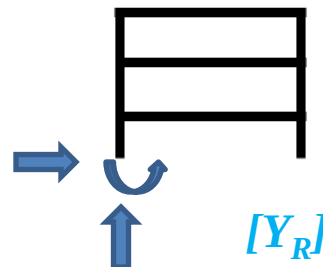
Séparation d'un problème en deux parties
(a) / (b) : source/récepteur



$$(f_c) = ([Y_S] + [Y_R])^{-1} (v_L)$$

$$(v_c) = [Y_R]([Y_S] + [Y_R])^{-1} (v_L)$$

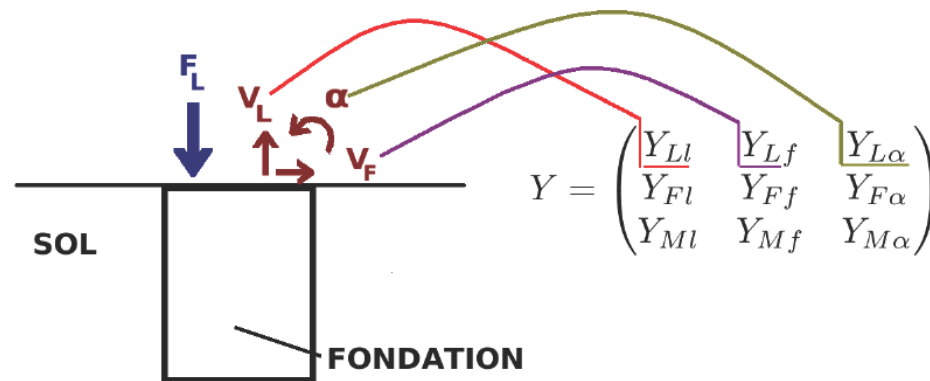
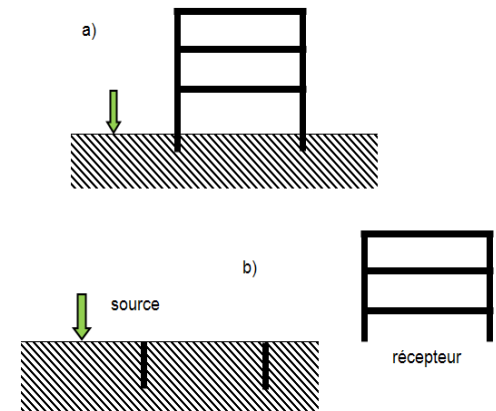
$$\Pi = 1/2 \operatorname{Re}\{ (f_c)^T (v_c)^* \}$$



Couplage

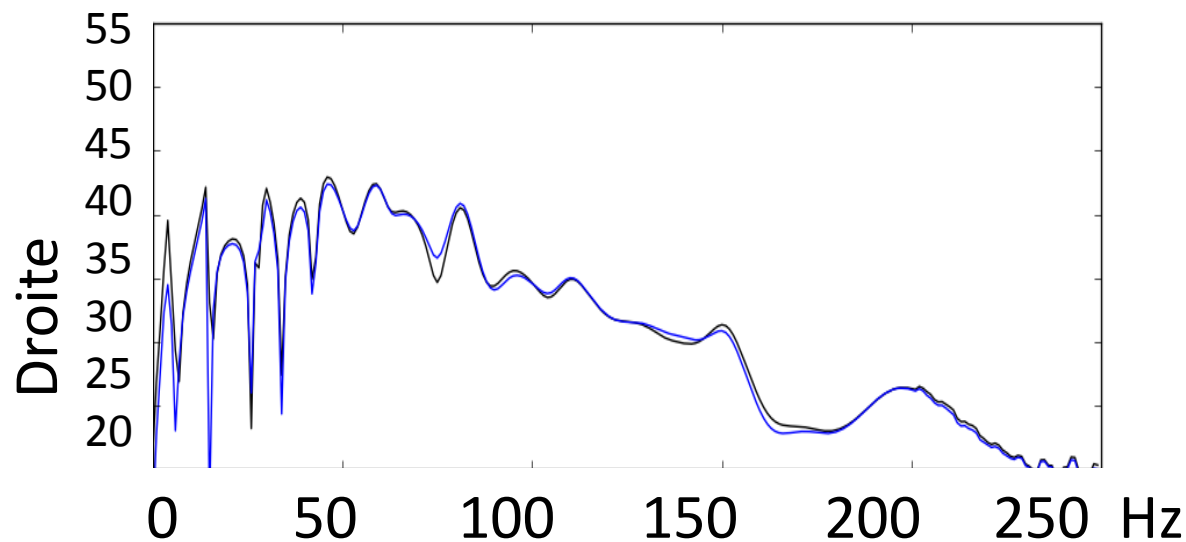
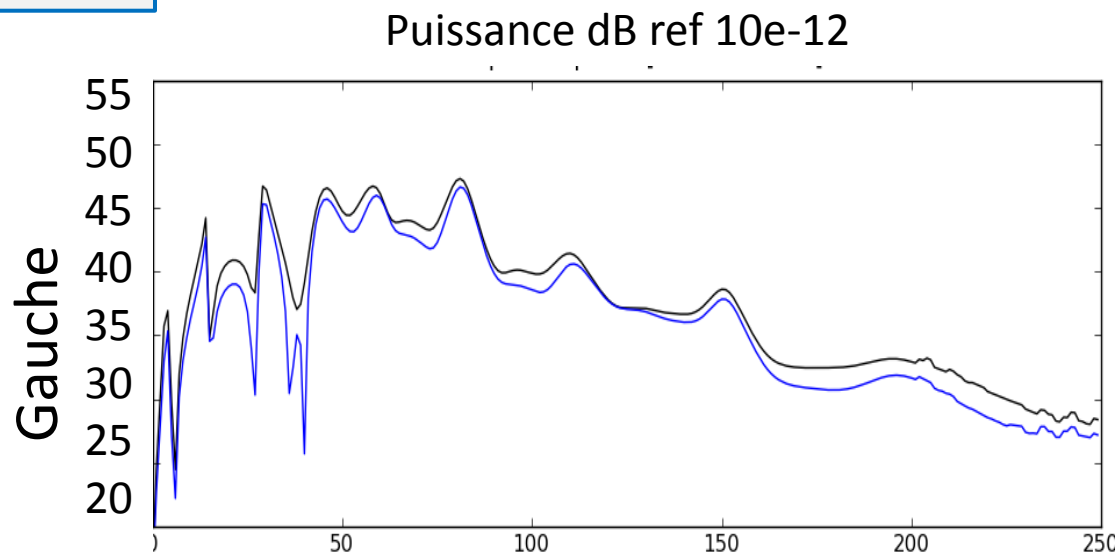
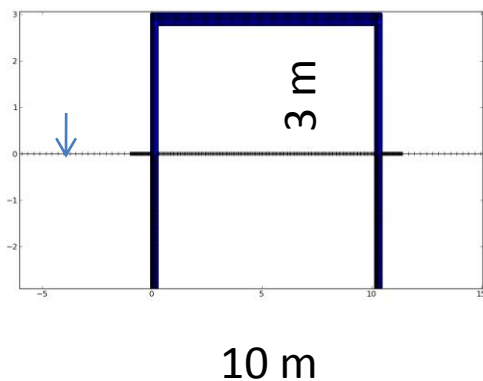
BEM/FEM (Mefisto) : sols + fondations

FEM (NASTRAN) : Bâtiments



Technique des mobilités: VALIDATION

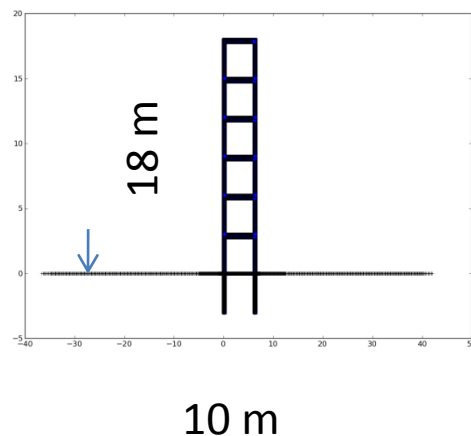
Approche par mobilités



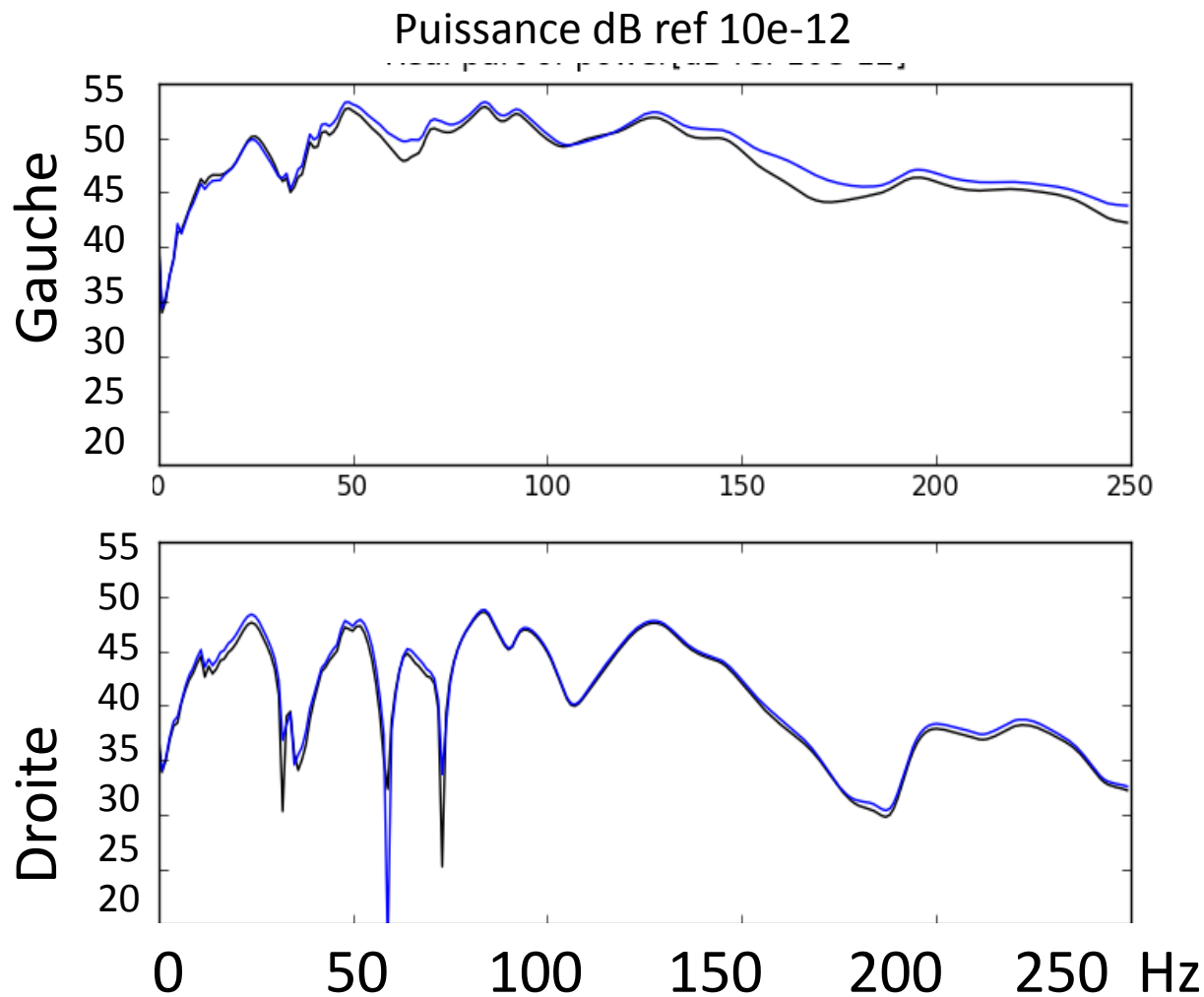
Puissance totale injectée :
méthode des mobilités
MEFISSTO

Technique des mobilités: VALIDATION

Approche par mobilités



Puissance totale injectée :
méthode des mobilités
MEFISSTO

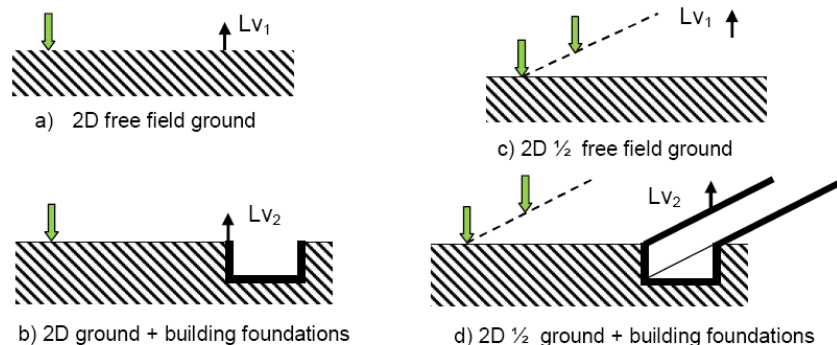


Immeuble proche
De voies
Mesures / calculs
Extrapolation

SNCF/CSTB

Validation expérimentale Ferroviaire *SNCF/CSTB/SATEBA*

1. Démarche: pas de bâtiment: recalage des vitesses en surface (BEM 2.5D)
2. Fonction de transfert: $H = LV(\text{sol seul}) - LV(\text{sol+fondation})$
supposée indépendante de la distance aux voies



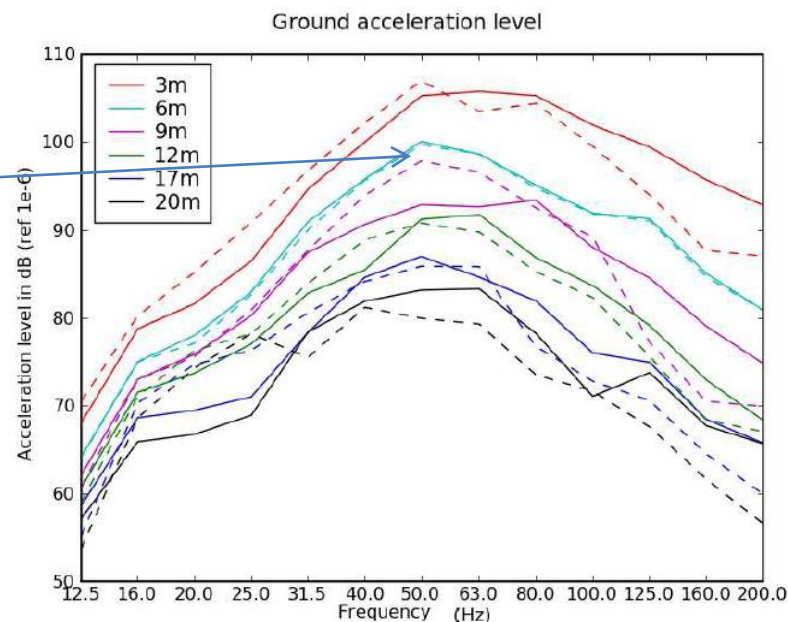
3. Extrapolation à d'autres cas: calculs BEM2D: recalage des calculs 2D avec:

$$H(2D) / H(2.5D)$$

Accélération en surface à d m de la voie
Calculs BEM2.5D recalés sur d=6 m

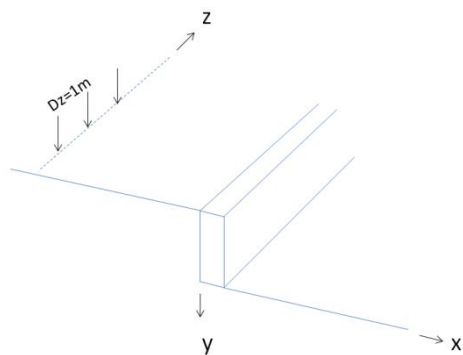
3 sols types homogènes au CSTB :

- standard
- plutôt dur
- plutôt mou



Atténuation avec la distance:
MEFISSTO 2.5D (___) mesure (- - -)

Importance du 2.5D / 2D



$$H = LV(\text{ }) - LV(\text{ })$$

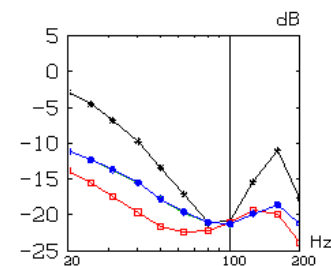
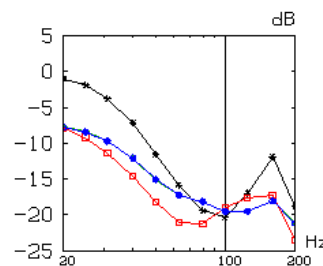
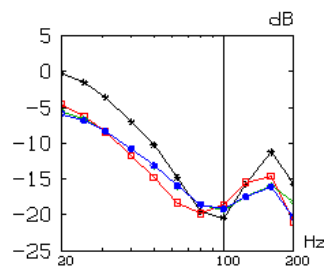
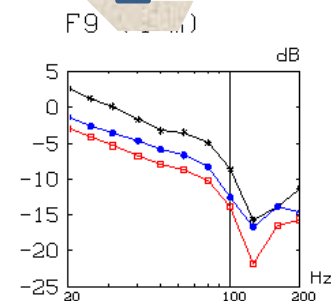
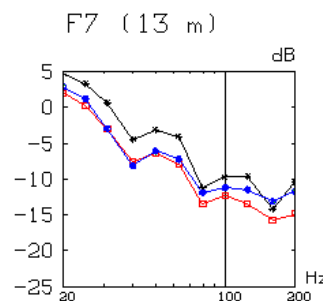
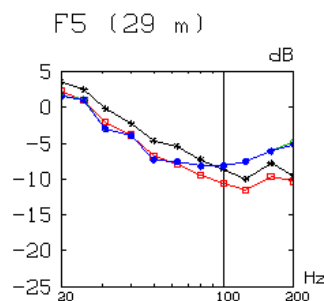


Horiz



Vert

$$H = LV(\text{ }) - LV(\text{ })$$

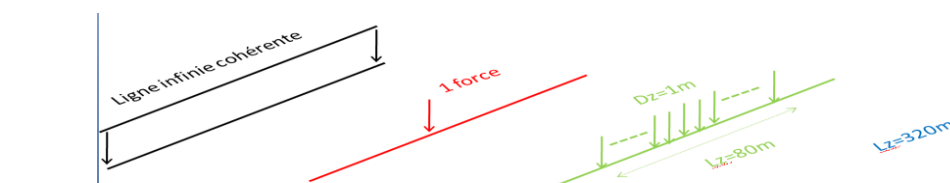


ligne cohérente

, source ponctuelle,

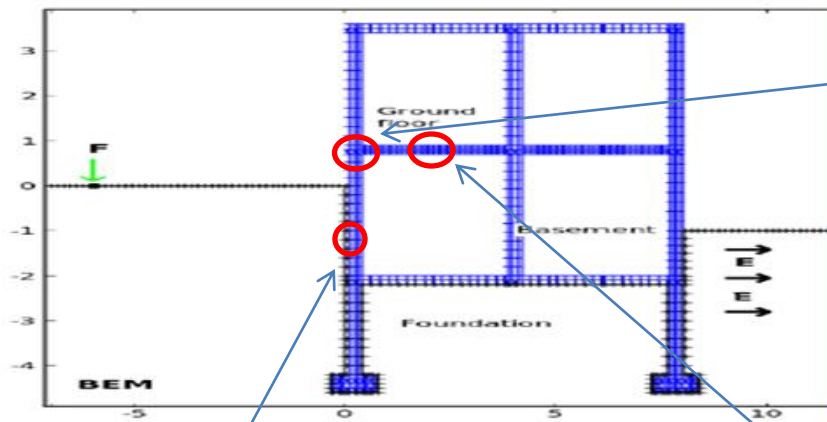
répartition de forces (tous les m) sur 80 m,

sur 320 m

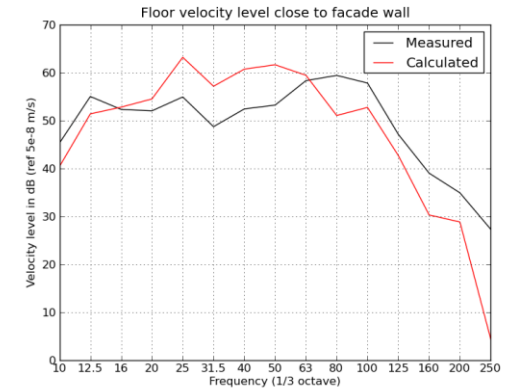


22- 23 Mars 2011

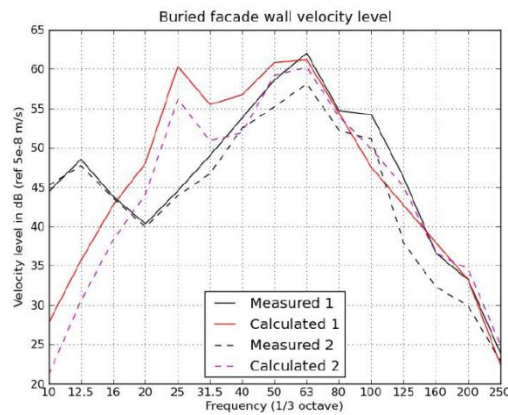
Comparaison mesures/calculs



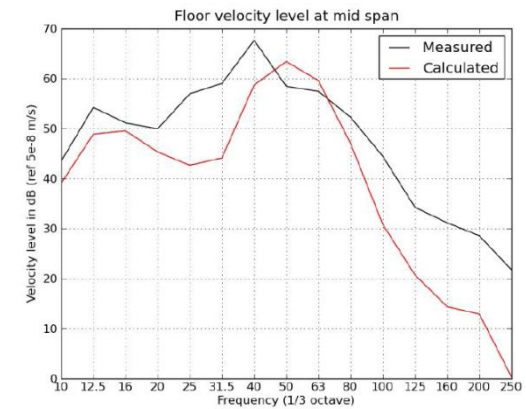
Mesure
Calcul



Vitesse verticale façade

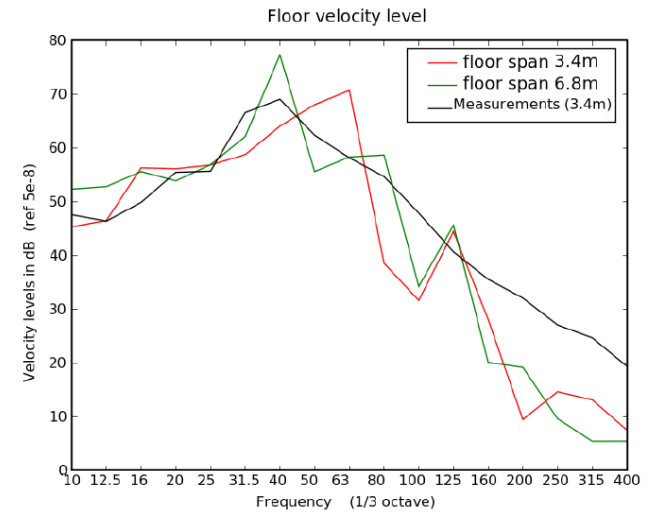
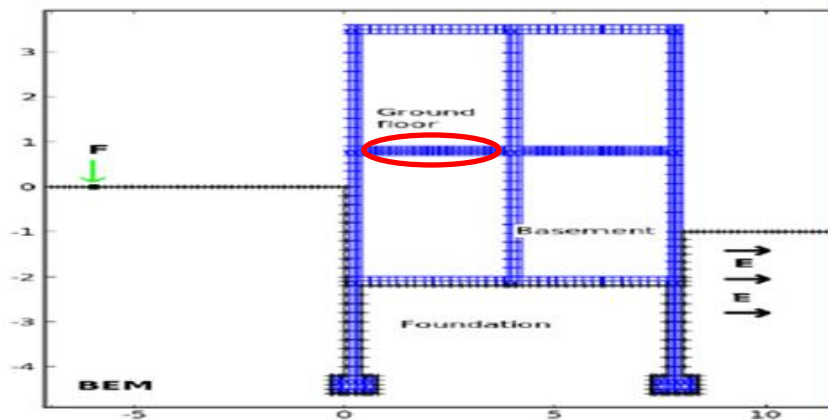


Vitesse horizontale: façade enterrée

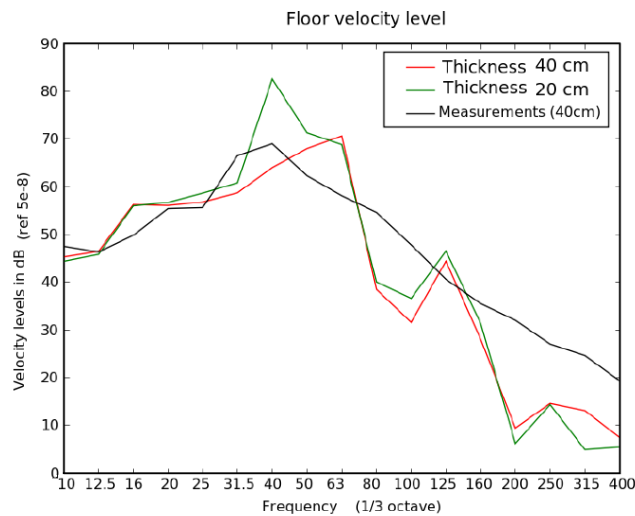


Vitesse flexion dalle (centre)

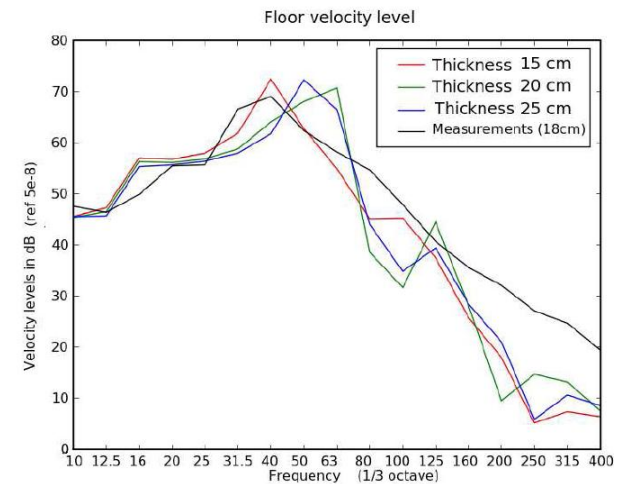
Influence de données géométriques



Influence de la portée des dalles



Influence de l'épaisseur de la façade



Influence de l'épaisseur des dalles

Indicateurs de gêne (exemple de la norme Norvégienne NS 8176) intégrés au modèle de calcul

Cas mesuré:

éloignement aux voies 6 m, h façade=40cm, h plancher=20 cm, portée 3.4 m

Indicateur $V_{w,95}$ obtenu pour les cas simulés

	Bâti mesuré (6 m)	Même bâti à 20 m	h façade 20 cm	h plancher 15 cm	h plancher 25 cm	Portée de 6.80m
$v_{w,95}$ mm/s	0.11	0.04	0.89	0.26	0.11	0.56

Class A ($v_{w,95} < 0.1$): vibrations non perçues

Class B ($0.1 < v_{w,95} < 0.15$): faible pourcentage (<10%) de gens gênés probable

Class C ($0.15 < v_{w,95} < 0.3$): environ 15% de gens gênés probable (recommandé pour bâtiments neufs)

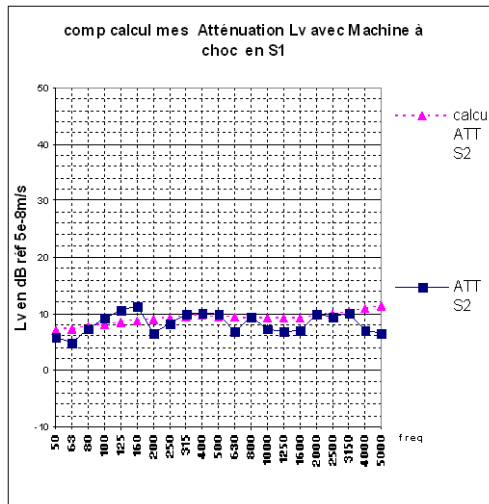
Class D ($0.3 < v_{w,95} < 0.6$): environ 25% de gens gênés probable (recommandé pour bâtiments existants si coûts d'amélioration pour passer en classe C prohibitifs)

Sources internes aux
bâtiments:

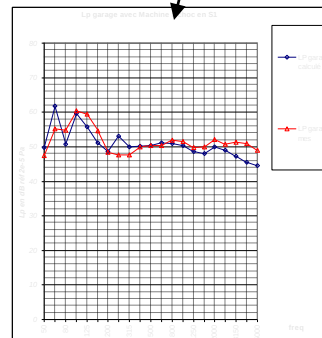
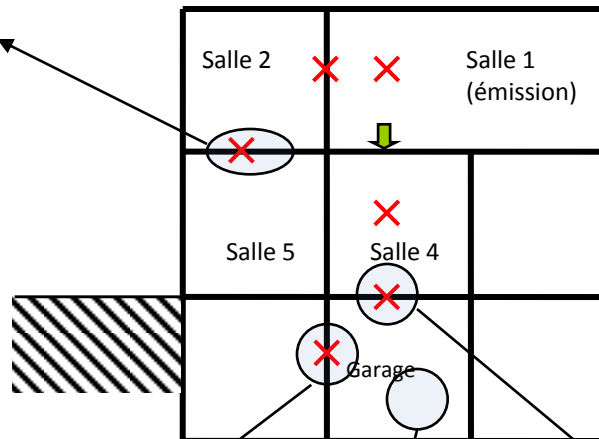
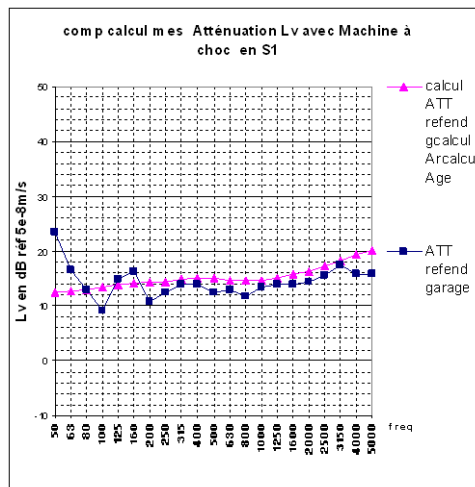
immeubles en
construction

BOUYGUES/CSTB

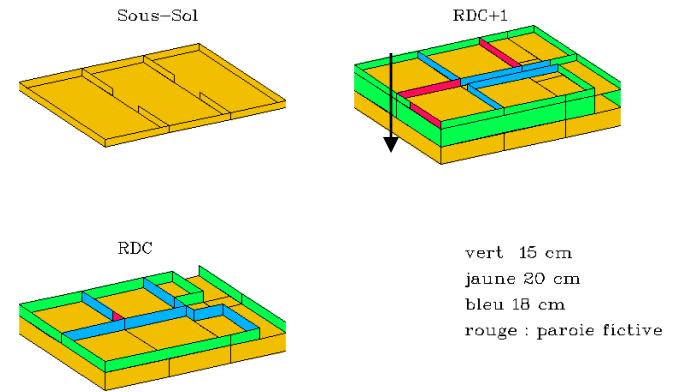
Niveau de vitesse



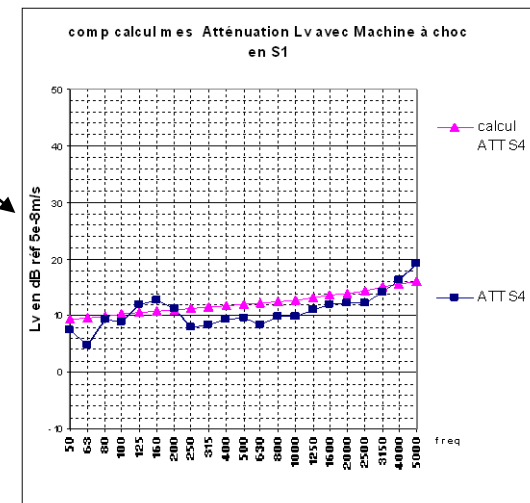
Niveau de vitesse



Niveau de pression

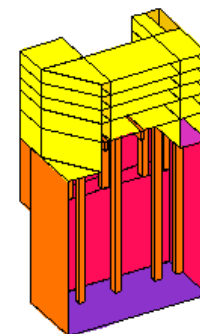
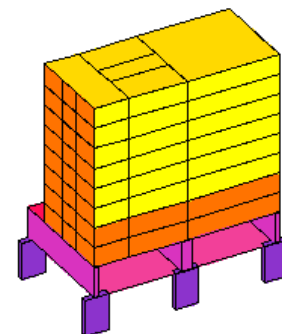
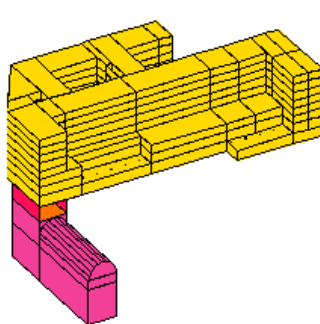


Niveau de vitesse

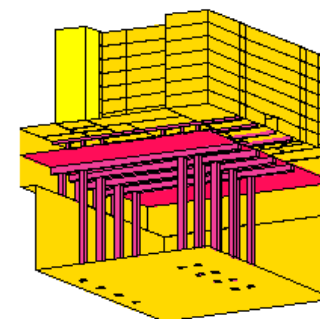
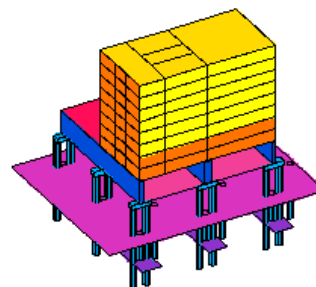
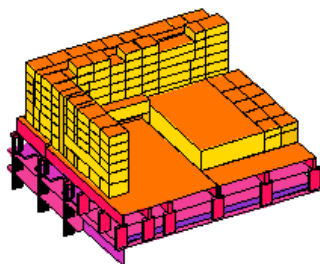


Grands Projets: gares Parisiennes

Eole



RERD

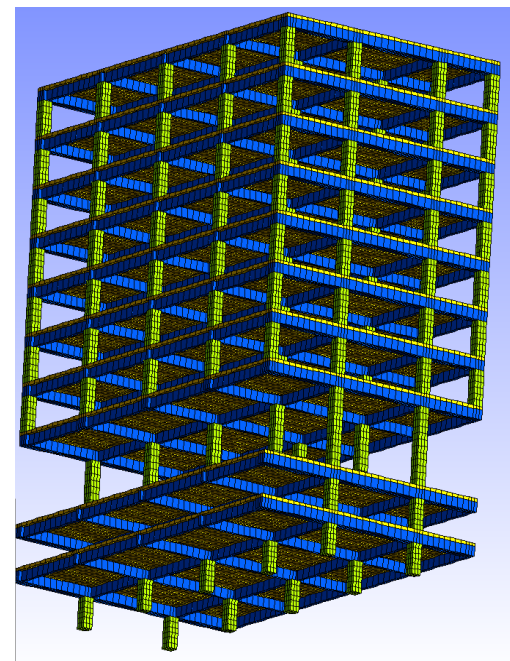
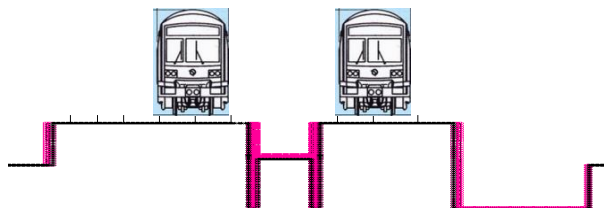


Dalle SEMAPA (Austerlitz)

SEA ; superstructures, modèles dédiés en infrastructures (ondes/SEA)

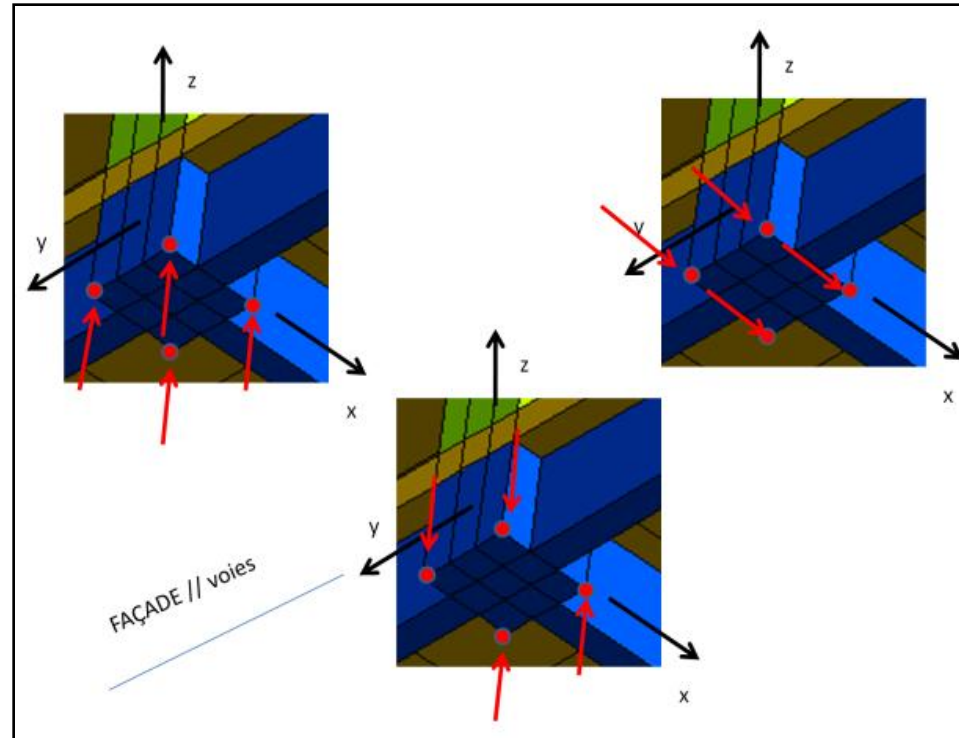
Grands Projets: Bâtiment voisin d'une gare ferroviaire

SNCF-Eole



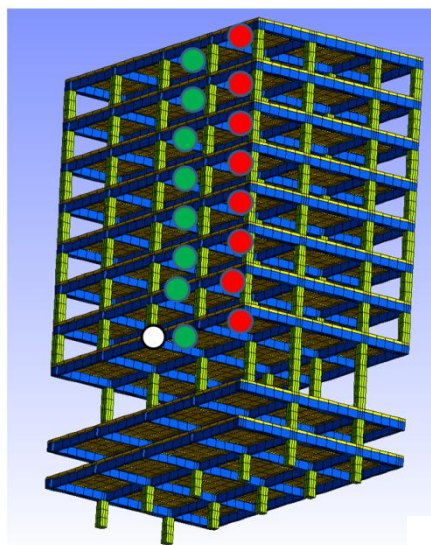
*Partie sous-terraines (calculs BEM) et
supérieure (calcul Nastran) d'un bâtiment*

Calcul des mobilités



Sollicitations en bas de superstructure permettant le calcul des mobilités

- Excitation
- Colonne 1
- Colonne 2



Excitation horizontale



verticale



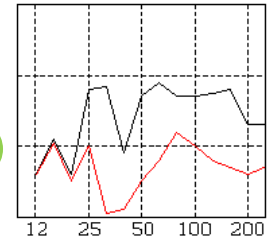
Colonne 1

Colonne 2

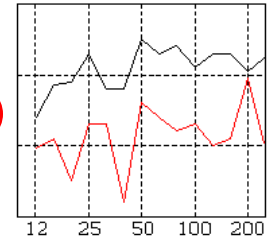
LV flexion de dalles

10 dB / grad

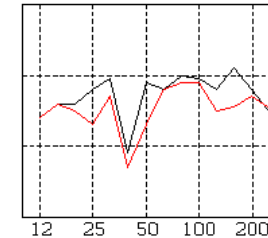
Excit Hor col 1



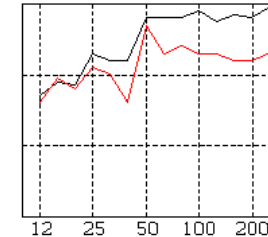
Excit Hor col 2



Excit vert col 1



Excit vert col 2



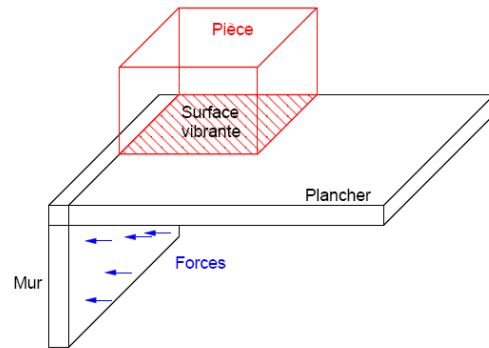
RDC

RDC+1

Rayonnement dans les volumes

Calculs

Thèse Guillaume COCQUEL (2005-2008) RATP/CSTB



$$\sigma = \frac{\Pi_{rad}}{\rho_0 c_0 S \langle v^2 \rangle}$$

where $\Pi_{rad} = \frac{\langle p^2 \rangle A}{4 \rho_0 c_0}$

Modélisation du rayonnement acoustique

Modèle analytique => vitesse V au sol

Rayonnement acoustique: Vsol, G réponse local => P

$$p(M) = \int_{S_v} j\omega \rho_0 \times v(Q) \times G_v(M, Q) \times dS(Q)$$

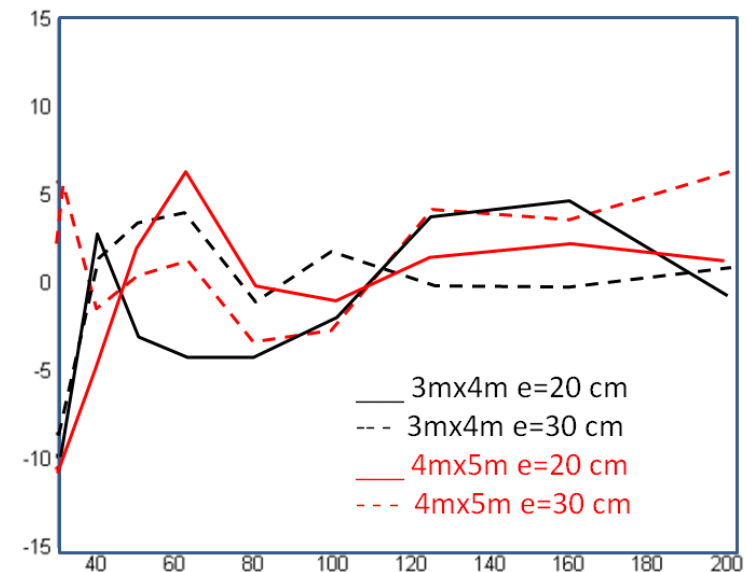
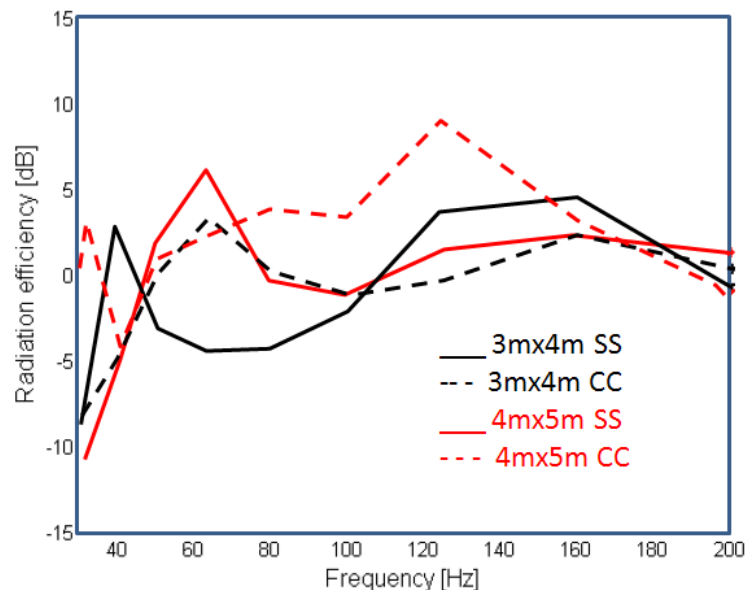
Tr => A A et P² => Π_{rad} => σ

Effet des caractéristiques sur le facteur de rayonnement

2 dimensions 3x4 m² et 4x5 m²

2 conditions limites: appui (SS) et encastrement (CC)

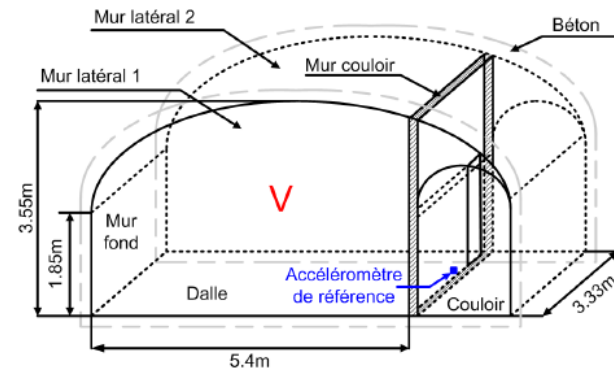
2 épaisseurs : 20 cm et 30 cm



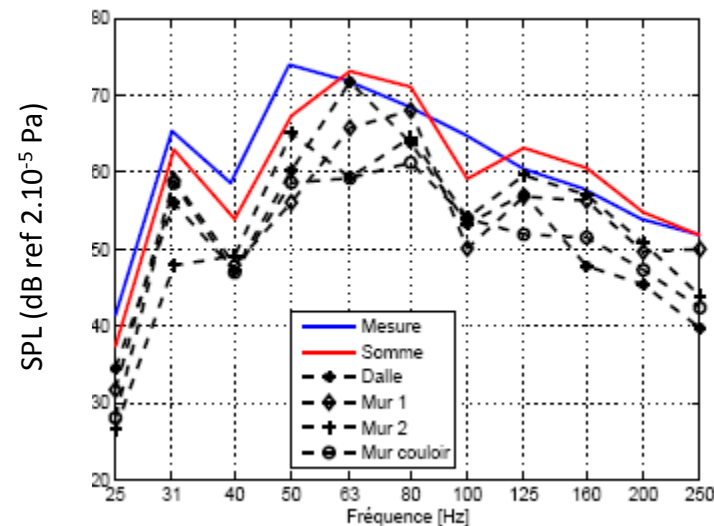
=> Estimation de plages d'incertitudes

Rayonnement dans les volumes - Mesures

Local technique RATP

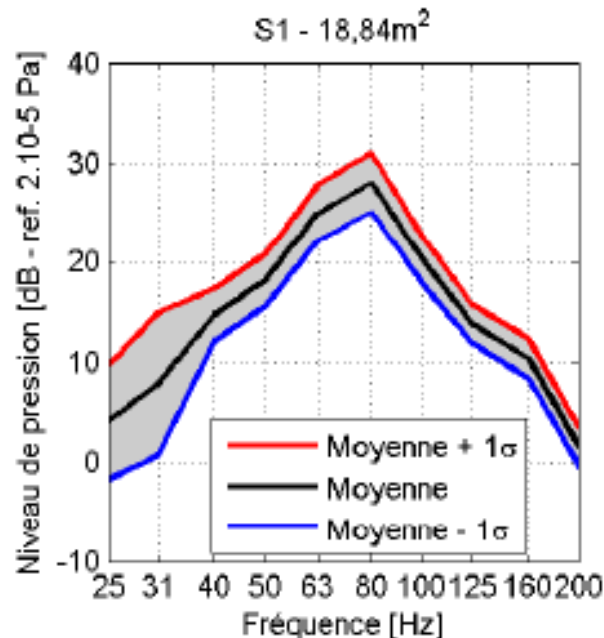


Mesures des vitesses
 LV , σ et $Tr \Rightarrow \Pi_{rad} \Rightarrow LP$

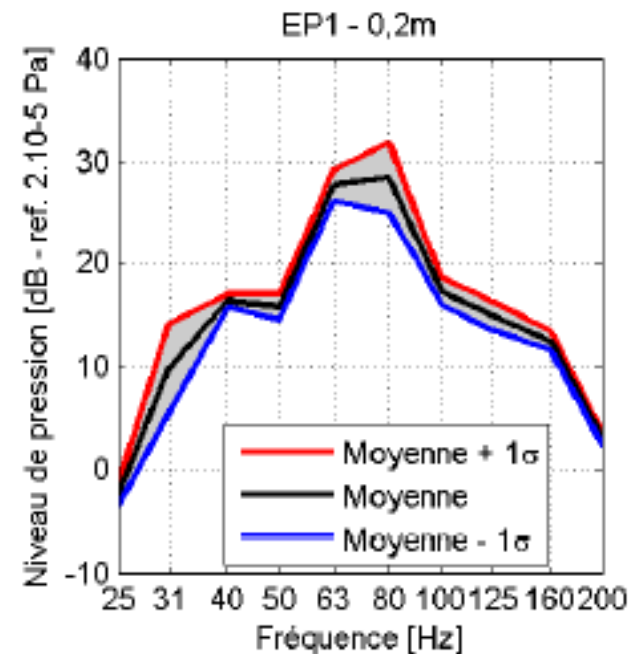


Rayonnement dans les volumes - variabilité

Incertitude issue des simulations



surface bloquée



épaisseur bloquée

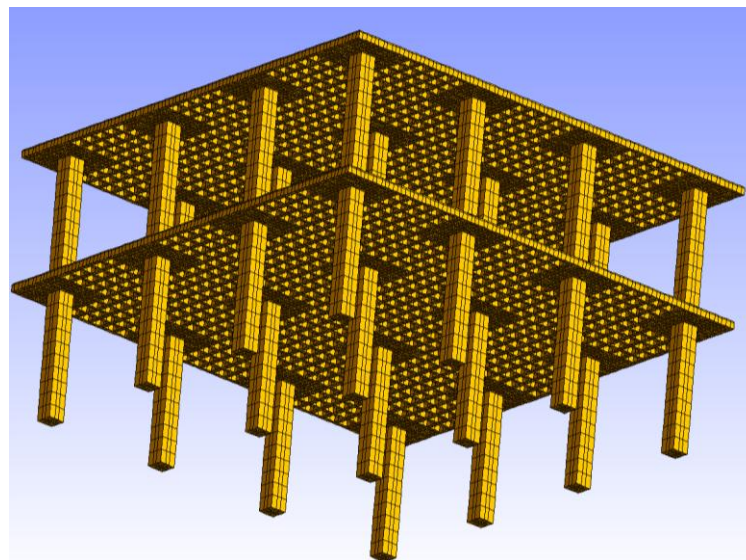
- Salle de séjour : S1 = 18,24m², S2 = 19,11m², S3 = 20,00m², S4 = 20,91m², S5 = 21,84m²,
- Hauteur : H1 = 2,5m, H2 = 2,6m, H3 = 2,7m, H4 = 2,8m, H5 = 2,9m, H6 = 3m,
- Epaisseur de la dalle : EP1 = 0,200m, EP2 = 0,225m, EP3 = 0,250m, EP4 = 0,275m, EP5 = 0,300m,
- Conditions aux limites : Encastré (CC), Appuis Simples (SS).

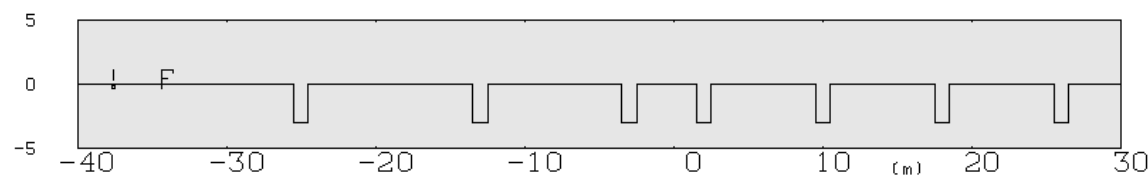
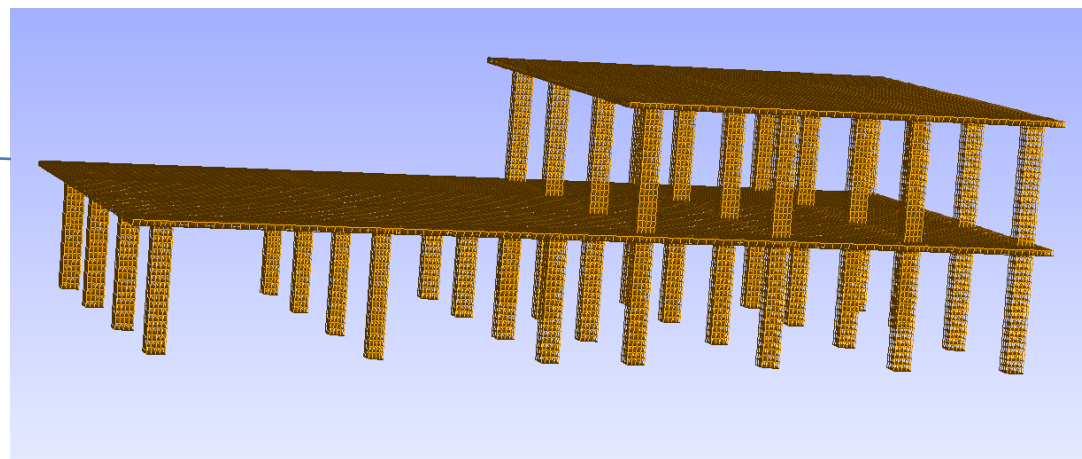
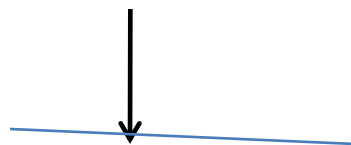
Entrepôts proches de voies ferrées: reconversion en logements (haut de dalle)

Réponse mesurée: **recalage du modèle**

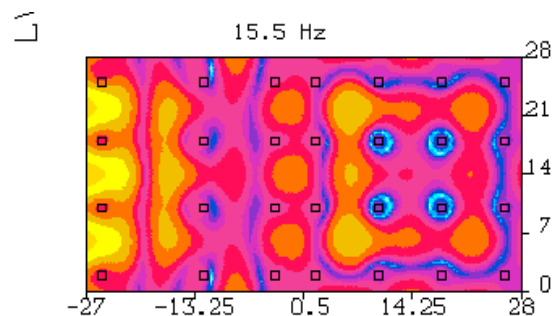
Objectif: prévoir l'effet des modifications structurales

*Portion d'un entrepôt
en sous-structure d'une
zone constructible*

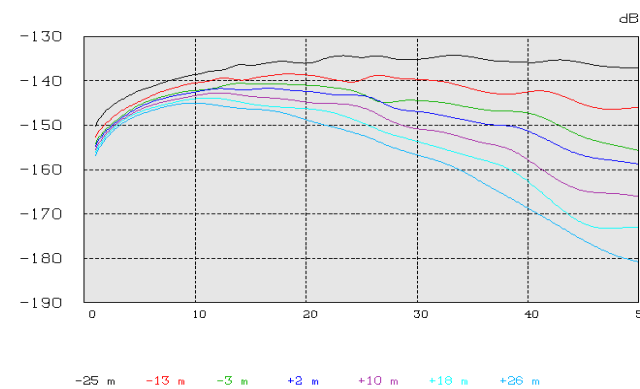




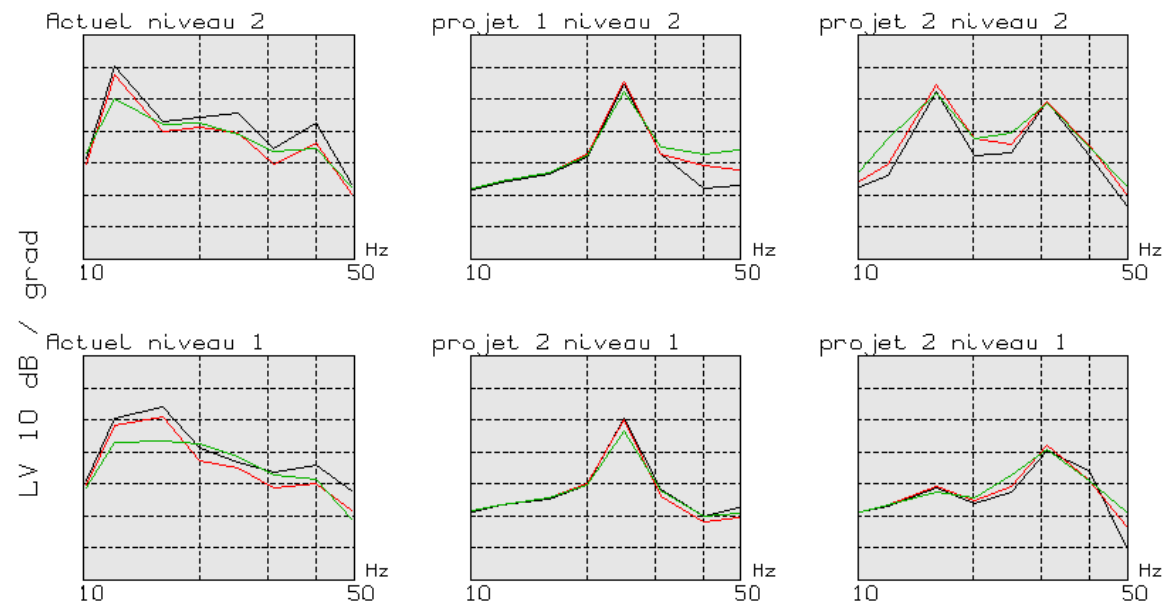
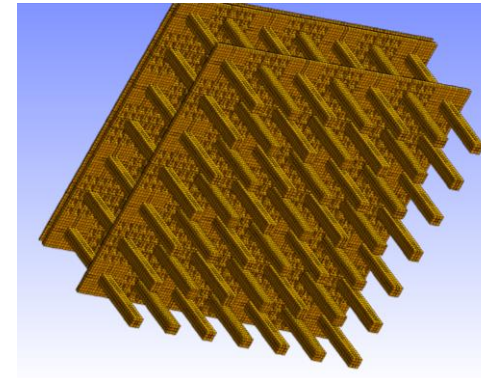
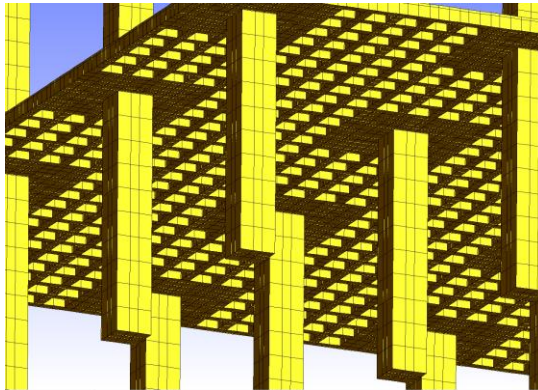
Calcul BEM de vitesses en haut de fondations



Niveaux de vitesse



Existant / projets



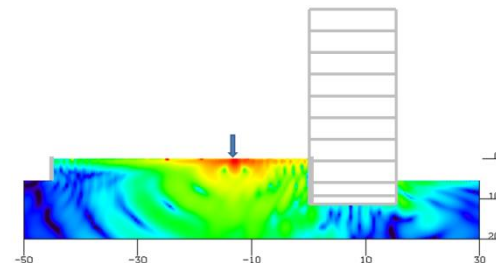
V au centre

22-23 Mars 2011

Vms 8x8 m2

Vms 27x27 m2

Conclusions et perspectives



- SEA: valide avec excitation en flexion dès 50 Hz
- Approches BEM/FEM
- Approche source /récepteur par mobilités: sol/fondation: BEM2.5D, (3D en cours)
structure isolée: logiciel du commerce (Nastran,..)
- Superstructure en 2D: résultats suffisants pour une étude paramétrique
- Etude de sensibilité aux variations des paramètres structuraux:
=> permet d'élargir les bases de données des modèles empiriques
- Estimation du bruit solide depuis des niveaux vibratoires
- Indicateurs d'exposition vibratoire en post-traitement
=> expression des modifications structurales en terme de variation de la gêne